

Research Article

Power Distribution and Possible Influence on Fuel Failure in WWER-1000

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The work is focused on the influence of investigation of some core heterogeneities and construction materials on the space power (fission rate) distribution in WWER-1000-type cores, especially from viewpoint of the values and gradient occurrence that could result in static loads with some consequences, for example, fuel pin (FP) or fuel assembly (FA) bowing and possible contribution to the FP failure root causes. For this purpose, experimental data and their analysis from two earlier performed measurements on light water, zero-power reactor LR-0 were used, concerning the relative radial power distribution determined by measurements in a WWER-1000-type core containing single FPs with homogeneous gadolinium admixture (Gd_2O_3) and the relative radial power distribution determined by measurements in FA situated on the periphery of a WWER-1000-type core neighbouring the baffle (thermal shielding).

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1. INTRODUCTION

The LR-0 reactor in the Nuclear Research Institute Řež plc is an experimental facility for determination of the neutron-physical characteristics of the WWER- and PWR-type lattices and shielding with UO_2 or MOX fuel. Exploitation of this facility is determined by maximum power of 5 kW and maximum thermal neutron flux density of $10^{13} \text{ m}^{-2}\text{s}^{-1}$, atmospheric pressure, and room temperature (or heating up to 70°C). The fuel consists of the shortened WWER-1000- and WWER-440-type fuel assemblies (FAs) containing the fuel pins (FPs) with UO_2 pellets (O.D. 7.53 mm, internal central hole 1.4 mm) having a Zr + 1% Nb cladding (O.D. 9.15×0.72 mm) with the active length of 1250 mm and enrichment of 1.6–4.4 wt.% in ^{235}U . The FAs can be arranged in a reactor vessel of aluminium (diameter 3.5 m, height 6.5 m); the criticality is controlled by moderator level (boron acid with concentration up to 12 g/L) and control clusters (B_4C pellets).

The most important applications on LR-0 reactor concern the nuclear safety and economy of the WWER-type nuclear power plants (NPPs) operation. In the frame of their modernization, a set of experiments has been performed on the LR-0 reactor, for example, with new type FAs

with various burnable absorbers arranged in appropriate configurations and cores of the both WWER-440 and WWER-1000 types including a number of experiments with FAs containing single FPs with Gd (Gd FPs) burnable absorber (Gd_2O_3) integrated into fuel (e.g., [1, 2]). Next experiments concerned the reactor pressure vessel dosimetry and they included measurements of the power (fission rate) distribution in periphery FAs neighbouring the baffle in WWER-1000-type cores (e.g., [3]). Results of power (fission rate) distribution measurements presented in [1–3] are used and analysed in this work.

It is well known that presence of single Gd FPs in reactor core results in a local depression of thermal neutrons in these FPs and corresponding gradients in neighbouring FPs. As for the baffle influence, thermal neutron gradients can be expected in neighbouring FAs, too. Similar situation can also be stated as for the power release and corresponding temperature.

It is also well known (e.g., [4, 5]) that neutron flux nonuniformity, gradients of the temperature, and neutron current can represent root causes of the FP/FA growth and bowing leading to local limitation of coolant flow, reduction of heat transfer, magnifying cladding corrosion, and pellet/cladding interaction (PCI). Therefore detailed

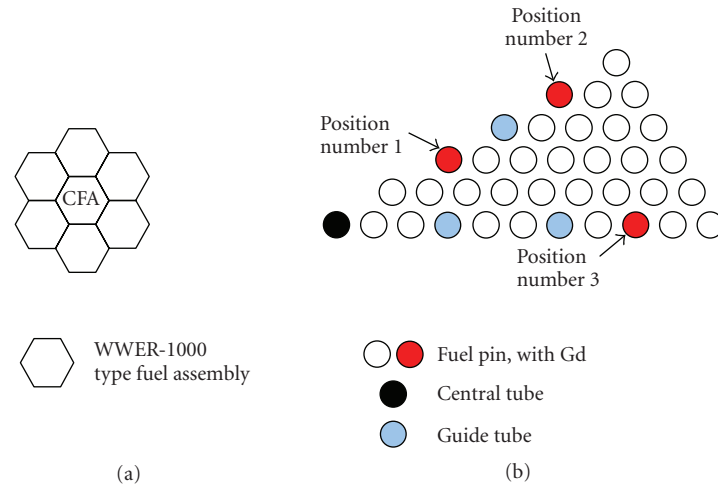


FIGURE 1: (a) Schematic arrangement of the LR-0 reactor core containing 7 WWER-1000 type-FAs with central FA (CFA) for Gd FP influence investigation and (b) the 30-degree symmetry sector of the CFA with 3 Gd FPs.

information about power distribution in FA containing single Gd FPs and in periphery FA neighbouring the baffle in WWER-1000-type core can be useful for above phenomenon investigation. Since such data cannot be obtained in the NPPs, some experiments on research reactors are provided.

As for the fuel performance reliability and fuel failure rates and root causes concerning WWER fuel, it was stated [6] that an overview on WWER fuel failure root causes identified during 1992–2002 shows that

- (i) besides a large number of unidentified causes, the most frequent cause is damage by debris;
- (ii) different from Western PWR fuel experience, fuel-rod-to-spacer-fretting does not play a significant role;
- (iii) at the same time there is a very high number of defected fuel where no failure cause is known.

In case of the PWR fuel the EPRI evaluation of 2004 on US PWR fuel failure rates shows [6] that

- (i) after a continuous decrease from 1980 to 2001, there is some increase observed in 2002 and 2003;
- (ii) the major contributor to fuel failure rates in PWRs remains grid-to-rod fretting;
- (iii) there is also an increase of fuel failures with unknown root causes that primarily affects optimised fuel designs with a thinner rod diameter.

The above information is in accordance with results concerning examination of 5 WWER-440 and 7 WWER-1000 FAs presented in [7]: causes of failure are debris fretting (54%), local overheating (15%), grid-rod fretting (8%), and “the cause is not determined” (23%).

2. AIM OF WORK

The aim of this work is providing some information about below heterogeneities and construction material influence on

radial power (fission rate) distribution in WWER-1000-type cores, namely, concerning the

- (i) single Gd FPs by means of power release in an FA containing these FPs,
- (ii) baffle by means of power release in selected FPs in neighbouring FA.

3. INFLUENCE OF SINGLE FUEL PINS WITH GADOLINIUM ON POWER DISTRIBUTION IN A WWER-1000-TYPE CORE

3.1. Experimental arrangement and conditions

The materials published in [1, 2] were used for this work preparation. Experiment was realised on reactor LR-0 with critical height of the H₂O moderator level being 266.10 mm (“0” level is at the lower end of FP active part), at atmospheric pressure and room temperature in a WWER-1000-type core shown in Figure 1(a), consisting of 7 FAs, each containing 312 FPs with 4.4% enrichment, whereas 18 FPs in central FA (CFA) were replaced by FPs with 3.6% enrichment containing 2.0% (by weight) of Gd₂O₃ admixture (Gd FP pellets with O.D. 7.50 mm, internal central hole 1.5 mm), arranged with FP pitch of 12.75 mm; the 30-degree symmetry sector of CFA with 3 Gd FPs is shown in Figure 1(b). More information concerning experimental arrangement and conditions can be found in [1, 2].

3.2. Results

The power (fission rate) distribution was determined by means of gamma scanning of irradiated FPs, measuring their gamma radiation in the energy range of 600 to 900 keV. The radial distribution (in a plane perpendicular to the core axis) was determined measuring FPs activity of 50 mm region of FP surface at the central irradiated part along rotating FP using corresponding collimator. Measurements

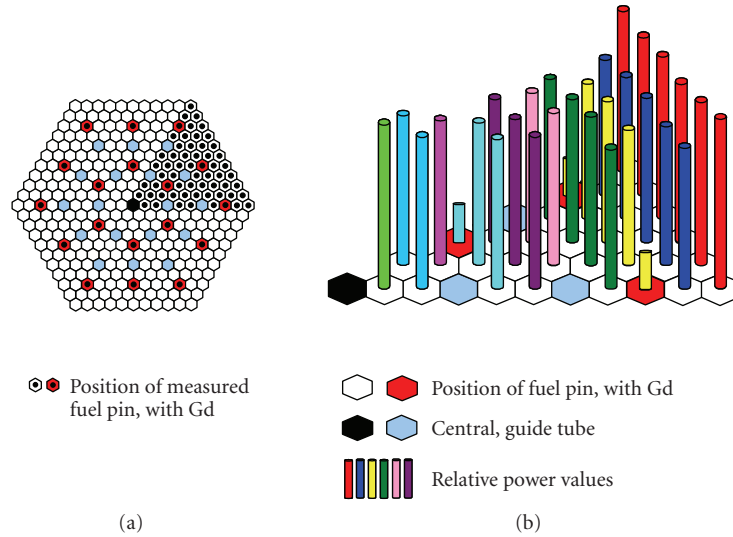


FIGURE 2: (a) Positions of measured FPs in CFA and (b) power distribution in the 30-degree symmetry sector of the CFA with 3 Gd FPs.

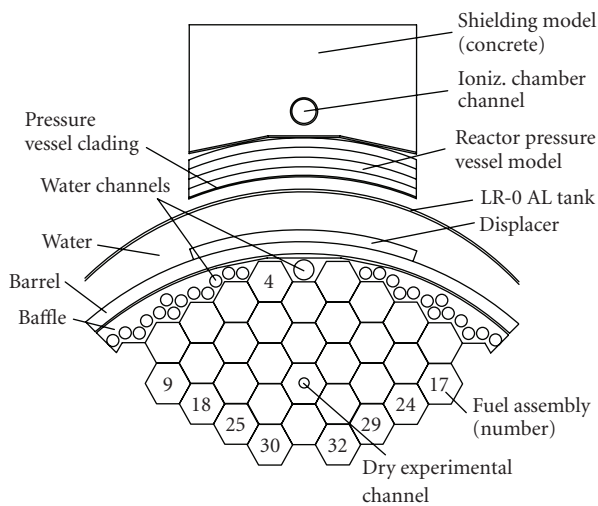


FIGURE 3: The section of the mockup by the XY plane.

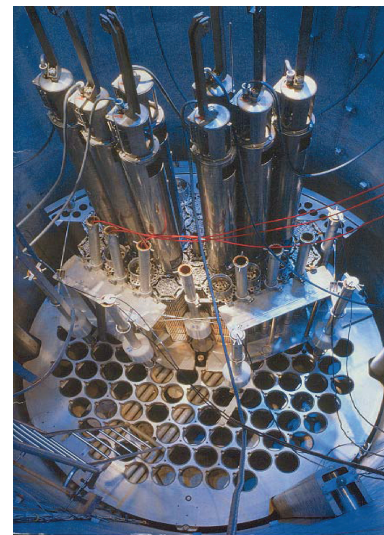


FIGURE 4: WWER-1000 mockup general view on reactor LR-0.

were performed in CFA at 74 FPs with positions shown in Figure 2(a); detailed results were presented in [2] and used for evaluation of power distribution in symmetry sector of CFA shown in Figure 2(b). As for this evaluation, absolute value of the difference of power release concerning two FPs in symmetry positions (Figure 2(a)) was calculated and related to the average of these two values and this was done for all above symmetry positions to check reproducibility of the results presented in [2]. The mean and maximum above relative differences are 1.1% and 3.8%, respectively.

Further experimental results were compared with calculations based on a code treats the two-dimensional, four-group diffusion equations using the so-called fine mesh method (each FP cell or absorbing rod cell is considered as one point) and presented in [2]. Results of calculations and measurements are in fairly good agreement: the mean value of the relative power distribution difference absolute values

is 2.4%; maximum positive and negative relative differences are 6.2% and -12.7%, respectively.

Finally the shape of the power distribution in the neighbourhood of a Gd FP can be characterised by the following ratio:

$$Q = \frac{\text{(average energy release at ring of 6 FPs around a Gd FP)}}{\text{(energy release in that Gd FP)}} \quad (1)$$

As for Gd FPs (Figure 1(b)) in positions nos. 1, 2, and 3, the following experimental Q_E /calculated Q_C values were determined: 3.718/3.553, 3.669/3.501, and 3.694/3.523 with

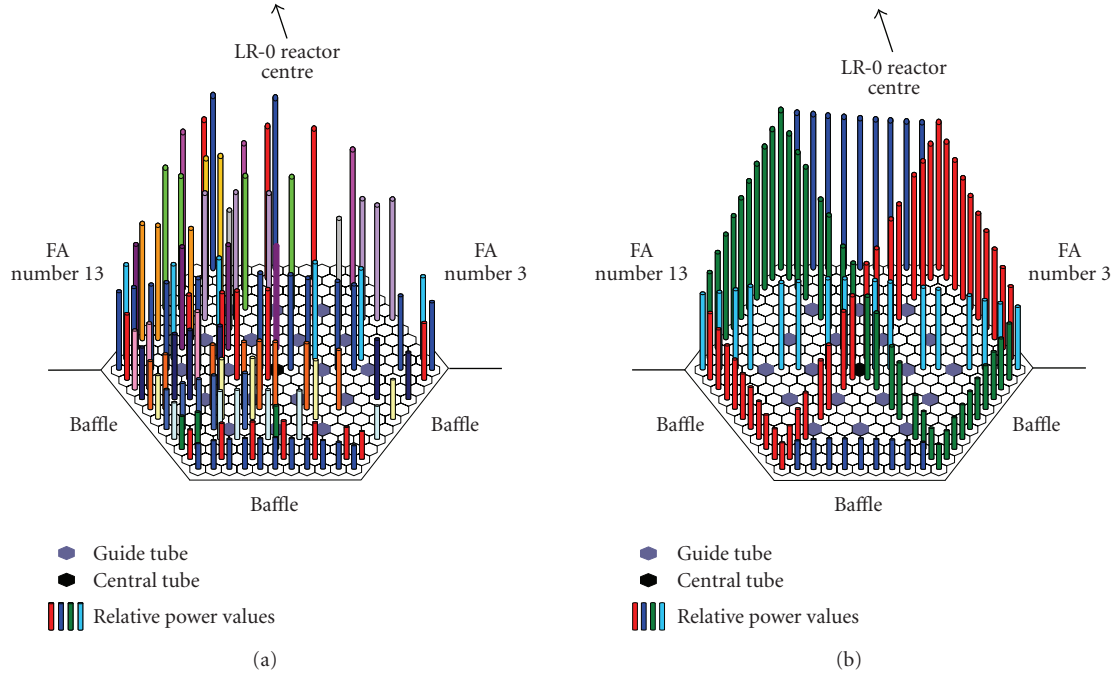


FIGURE 5: (a) Experimental and (b) calculation power distribution values in selected FP positions in FA no. 4.

relative difference $d = 45\%$, 4.7% , and 4.7% , respectively, where

$$d = \frac{(Q_E - Q_C)}{[(Q_E + Q_C)/2]} \quad (2)$$

A fairly good agreement between measured and calculated power distributions can be stated, given by above mean value of 2.4% , as well as between experimental Q_E and calculated Q_C quantities given by above difference d being about 4.7% for all three Gd FP positions. The power release depression in Gd FPs can be characterised by the value of $1/Q$ with corresponding values in positions 1, 2, and 3 being 26.9% , 27.3% , and 27.1% , respectively.

4. INFLUENCE OF BAFFLE IN WWER-1000-TYPE CORE ON POWER DISTRIBUTION IN NEIGHBOURING FA

4.1. Experimental arrangement and conditions

A 60-degree symmetry sector of WWER-1000 mockup in radial direction was realised in the LR-0 reactor at 4.6 ± 0.1 g/l boron acid concentration in moderator with critical height of 1500 mm ("0" level is at the lower end of FP active part), at atmospheric pressure and room temperature—Figures 3 and 4.

This mockup represents the core periphery and radial shielding heterogeneities of the WWER-1000. The core loading was chosen to imitate neutron source in $R - \theta$ geometry with following FAs no./enrichment: 2 FAs nos. 9, 17/3.3%, 6 FAs nos. 18, 24, 25, 29, 30, 32/3.0% and remaining 24 FAs with 2.0% enrichment (more information in [3]). The materials published in [3] were used for this work preparation.

4.2. Results

Influence of the baffle was investigated by means of power (fission rate) distribution in neighbouring FA no. 4, using gamma scanning of irradiated FPs, measuring their gamma radiation of the ^{140}La with energy 1596.5 keV. The radial distribution (in a plane perpendicular to the core axis) was determined by FPs activity of 50 mm region of FP surface at the central part along rotating FP using corresponding collimator.

Results of the power distribution measurements carried out in 107 FP positions in FA no. 4 are presented in Figure 5(a). Power distribution values were determined with mean and maximum relative errors being 3.2% and 5% , respectively.

Obtained experimental values were completed by calculations carried out in all 312 FA positions [3]. They are illustrated by values in selected FP positions in Figure 5(b).

Presented results demonstrate depression of the power distribution in FA no. 4 neighbouring baffle that can be characterised by the ratio of the power distribution mean values in two opposite FP rows in FA no. 4 to- and outwards the baffle. The depression, for example, the above ratio of about 19% , can be stated.

5. DISCUSSION

As for gadolinium influence, the obtained results have limited information relevance since the experiment was realised in 1990 at special conditions as mentioned above and therefore these results can differ from ones corresponding to the real NPP cores because of dependence, for example, on enrichment and dimensions of the (Gd) FPs, Gd_2O_3

contents, FP pitch, and Gd FP positions in FA, boron acid concentration in moderator, temperature, pressure, and so forth.

Similar situation can also be stated concerning the baffle influence. Further, a less influence of baffle on power distribution (depression) can be expected in an NPP core (with real WWER-1000 dimension) because of less dimension of LR-0 core used for investigation.

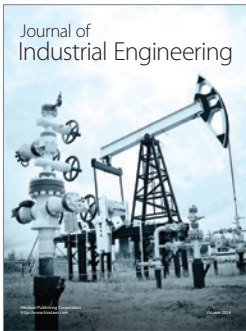
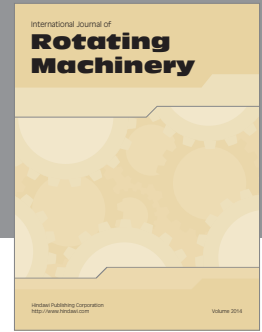
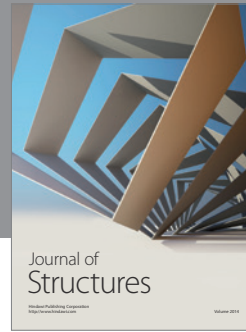
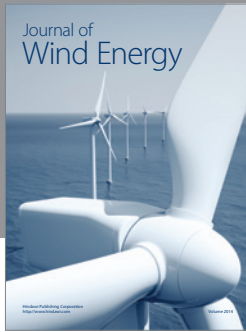
6. CONCLUSIONS

On reactor LR-0 in WWER-1000-type cores the influence of single Gd FPs and the baffle on the space power (fission rate) distribution was investigated. A strong power release depression of about 27% in a single Gd FP (3.6% enrichment, 2.0 wt.% Gd_2O_3) was determined, given by the ratio of energy release in that Gd FP and average energy release at ring of 6 FPs (4.4% enrichment) around this Gd FP. As for baffle influence in neighbouring FA, the power release depression of about 19% was estimated, given by the ratio of the power distribution mean values in two opposite FP rows in this FA to- and outwards the baffle.

The above results can be utilised for obtaining some information for the temperature gradients and resulting loads estimation in FPs neighbouring a Gd FP and in FA neighbouring the baffle to consider possible contributions of these loads to the FP failure root causes.

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